

UNIT-T

WIRELESS

CAR

Wired channels.

stationary

wireless channels

CH

CHANNELS

+

predictable

→ Kaneria, path b/w fix
& Ry

can vary

from

simple LOS

to one

that

is severely
obstructed

*

spe

ed

by buildings, mountain

+ pliage

д

motion impacts how
rapidly the rigral

level

jades

as a mobile terrenal moves in

signal

Large-scale propagation

Models - pudicts the

strength you

an & are useful

is

Small-scale (a

%7

mean

مقسم در

arbitrary $T_0 - R_0$
seperation distance

estimating
of a team
mitter

Fading
Models -

the received

the radio

Courrag
e

aria

characterize the rapid
fluctuations

signal
strength

over

very

short travel

distances (wavelengths) a short travel
duration

=>

As a

mobile moves

or

very

small distances, the
instantaneous

received signal strength may fluctuate
rapidly giving rise to small-scale fading.
This is because the received signal

coming from

differer durctions. => In small scale fading, the received signal power may vary

is sum

byr

من

of many

contributions

much

as there

a four aiders

f magnitude

(20

20 01

40 de) when the receiver is moved only by a fraction of a

wavelength.

= As the mobile

moves

away from the
Tx

larger
distances
gradually
decrease

the local

average

received

na

mech

signal will this local average signal

it is this local

level that is predicted by large-scale
propagation

models.

Free Spice

Propagation Model

→ Free

space propagation model is used to predict received signal strength when the transmitter and receiver have clear, unobstructed LOS path between them.

Ex: satellite communication

⇒ The

microwave LOS links.

free space power received by which is separated from

from a

radiating transmitta

a receiver antenna

antenna

by θ_a

distance d ,
giver

by

the
Friis

free
space

equatio

n.

$$Pr(d) = \frac{P_t A_z A_r d^{-2}}{4\pi d^2}$$

$$(4\pi T) da \cdot L$$

P_t -
transmitted

power

$P_r(d)$ - received power

which is a

a

function

of

T-R separation

G_E

transmitter antenna
gain

We recover antenna

gain

Лоло

L- system low
factor

расво

я

1- wavelength in
meters

λ

⇒ The gain

of

aperture, A_c ,

by

⇒

an antenna is related to its
effective

A_c is related to the
physical singe

$$A = 4\pi A_e$$

te
⇒ The effective
aperture A_c

q

the antenna

⇒ The d is related to carrier

d

गन

⇒ P_t & P_r is expressed in
опс
сос

by

делед.

бу

same units

little are

dimensionless quantities

• → The miscellaneous losses I

are

usually due to
transmission

line attenuation, filter losses & antenna
larger in the Communication system.

→ Friis free space equation shows that the
received

• =>

power falls off
we received Friis

20 dB /
decade .

as

the

square of

d

$T-R$

separation
distance.

power decays with distance at a rate

An isotropic radiator is an ideal antenna which radiates

with unit gain equally in all directions, & is used to reference antenna gains in wireless systems.

power

* The effective isotropic radiated power (EIRP) as defined

as

$$EIRP = P_{avg} G$$

represents the maximum radiated

power

& available from

it in the direction

of

max. antenna
gain

is used instead

a3

* In practice, effective
radiated

power
(ERP)

the maximum

radiated

power

as compared to **a**

EIRP to denote the

haly

-wave

dépol
e

Antenna

⇒ The

موصل

loss represents signal attenuation
as measured in dB, & is defined

path positive
quantity

the difference between the
effective transmitted

received

power.

$$PL \text{ (dB)} = C_0$$

- to

log

$$\cdot \text{Log } P =$$

$$= -C_0 \log$$

Pr

power

At head

(4T)♡ da

Designing antennas to have unit gain,
ikame

=> The

$$- \text{PL (dB)} = 10 \log B = 10 \log \left(\frac{4\pi r^2}{\lambda^2} \right) \text{ dB}$$

for
field

Pe

$$\left[\frac{P_e}{4\pi r^2} \right]$$

a

44

& the

(0 Fraunhofer region,
of a transmitting antenna is defined as
a the region

as a the region behind the
far-field

distance,
of

where $D =$

$d_f =$

$$\lambda^2$$

largest physical linear dimension

Additionally, d must satisfy

+

of
of

?

949

40.

کندا .

the antenna

$E_n \approx 0$ does not hold for $d \ll \lambda$.

Thus large scale

propagation
models are a

close in distance, d_0 ,
known as

received

power reference
point.

$P_x(d_0)$

=

$P_t A_t d^{-2}$

$d_z d_0 d_g$

$(4.5) 2$

dork

Comparing
with O

⇒ Because

$$P_r(d) = P_2(d_0) (d_0),$$

dz dozdy

of laye dynamic range dynamic
range of received

power leads, often
dbm

↳ a dow cerits

vo log [Pr (do)]

+ dolog (do) ,

djsdad

[o

गत

$$Pr (d) \text{ dBm} = 10$$

⇒ The distance do

fire

using

antennas in 1-2 GHz

range

is

typically

y

chosen to be

in

in indoor environment

low

gain

of 100m

Find the

dimension

of

a 1 km in outdoor.

W32

Fraunhofer distance you **an**
antenna with **mook**.

+ operating frequency
of 900 MHz. If
calculate the path
loss.

Im

Antennas have unutilized

Solar

TO

Cuvier

find

gain,

$D = Im$

$f = 900 \text{ MHz}$

y

of =

2D 2

λ

$$P_2 \text{ (dB)} = -60$$

وما ما

$$de (4\pi)$$

$$2 d^2$$

$$1 =$$

$$3 \times 10$$

$$= 0.33$$

$$900 \times 0.06$$

s

$$2(1)$$

$$3 \text{ dj so} 2 = 31) 2$$

$$= 6m/$$

$$P_2 \text{ (dB)}$$

=

- Co

$$0.33$$

of a transmitter
 produces
 transmit power in

$$\frac{P_{out}}{P_{in}} = \frac{4532}{2}$$

$$= 47 \text{ dB/}$$

So w

↳

log

$$(0.33)^2$$

$$(45)^2 =$$

$$(6) =$$

π

2

of power,
express

the

dBm & d₀. I **sow is**

applied to a unity gain antenna with
900MHz carrier frequency,

find the

Received

power

100m

power

in dBm at a

**free space
distance**

from the antenna. What is P_2 (10 km)?
 Arovone
 unit your for receiver
 antenna.

Sol

mist 120

m og

Cuven : $P_t = 50W$

$f_o =$

900MHz

$d =$

$d =$

TO

find

100 m

... D PE

(dBm) .

ii) P_z

(dBw)

dii) $P_{r\text{ford}} = 100\text{m}$

los P_e

(dBm)

v) P_r

for

$d = 10\text{km}$

Зхrot

Я пожов

20.33

31

ASCA

;)

P_t (dBm)

=

=

to log

$[P_t(\text{mw})]$

$$\text{to } \log [00 \times 10^3] = 46.93 \text{ eadem //}$$

$$\text{ii) } P_t \text{ (dBw) } =$$

co

co

$$\text{Log } [P_t \text{ (w) }]$$

$$= 20 \text{ (og } [50] =$$

$$16.9 \text{ dow/}$$

$$\text{ii) } P_r$$

$$P_t G_t \text{ had}$$

=

$$(4\pi)^2 d^2$$

L

- in) $P_e \text{ (dBm) } = \text{to } \log [I_a \text{ (onw) }]$

• v)

Considering

المعاني

=

ما

CO

СОД

[Be

50 (1) (1)

(0.33) (49) 2

(100) = (1)

(100) = (1)

=

3.44x10^{-b}

w

= 3.44 x 10

$$\text{to } \log [3.44 \times 10^{-2}] \\ == 24.6 \text{dBm/}$$

doz 100m + d=c0km,

$$P_a(d) = P_a$$

(de) (day
(oo)

$$\Rightarrow P_x(10 \text{ km}) = P_e \\ (100) \times 100$$

$$=-24.6 \text{dBm}$$

10x
Xx

2017

Px

2%

開

P2 (6) dan = to log [P2 (de)] + as log (1)

ما

ما

CO

Д

(do)

0.001 W

mw

d

$$= L_{0 \text{ ley}} [B. (4)] + \text{dolog} (2)$$

Pe (10
km) dBm

$$= \text{toto } \mathbf{Pe} (100) \text{ dBm} + 20 \log (10000)$$

$$= \text{cotog} E - 24.6 +$$

$$20 \log (100) =$$

СОД

64.5dBm

И

$$20\log(1) = -64.5$$

dBm/

Ground Reflection (Two -
Ray). Model :))

→ The two

-ray **reflection** model **is**

based **on** ground wave optics & Considers

both direct path + ground reflected

propagation

path b/w Tx & Rx

- This model is found to be accurate
for predicting layer

scale signal

strength for

mobile radio

systems

in urban environments

over distances

a

several kilometers

ht

Fi

As well as

LOS, micwell channels

ELOS

ETOT =

$$E_{\text{los}} + E_{\text{g}}$$

R

Lá

$$E_{\text{x}} = E_{\text{g}}$$

Qi

do

止

-d

K

=> The total E-

=> If -

ϵ_{TOT}
- fultd,
 $FTOT$, is

$$\epsilon_{TOT} = \epsilon_{LOS} +$$

Eq

E_0 - free space E-field at
reference distance d_0 , then for $d > d_0$,
the free space propagating
E-field

E_0

Cos

$$E(d, t) = \underbrace{E_0}_{\text{Envelope}} \cos(kd - \omega t) \quad (6-1)$$

مو

Where $E(d, t) = \underbrace{E_0}_{\text{Envelope}}$

— envelope

E_0

d

спосворя

су

E-field

d

=> Two

propagating

waves arrives *at* the Reng

* direct

wave

*

--

reflect
ed

wave

=> The I-field due
to

$E_{LOS}(d', t)$

=

travels a distance d'

travels a

distance d''

205 Component at

Rx

W to do ot

d'

$\cos(voc$

$(t-d))$

دها

The E-field for ground replented

wave

$$E_g(d'', t) = p E_{od}$$

$$C_{oo}(\omega c(t-d''))$$

where

Γ

=) The total

d''

CA

lection

coeff. p_e ground.

eglec

a

μ

Electure fired FroT

(d, t) is

Ry مشد

$$\text{EnoT } (d, t) = \text{Fodo los / we } (t - d') + (-1) \underline{\text{Eodo Cas}} (we (t - d''))$$

d'

مها

(we

d''

[Assuming perfect
horizontal E-fired
polarization ($\nu = -1$)

=)

=>

Using

Method

g-images

d!

ht he

ht

ht

ht the

d''

R↑
he

The path
differences,

between Los &

ground
reflected

paths

F

$d \gg \lambda$ hothe, wing

taylor series

is

$$s = d'' - d' = \sqrt{(h + h_e)^2 + d^2} - \sqrt{(h + \text{pha})^2 + d^2}$$

approx

$$s = d'' - d' = 2h \tan \theta$$

d

=) The phase diffr. O_S b/w tws E -field components **in**

$$OD = \frac{1}{c} \int_0^L n(z) dz$$

The time delay E_d b/w arrival

$$td = \frac{1}{c} \int_0^L n(z) dz - \frac{L}{c}$$

two Components in

O_S O_S

=

$+c$ c c

c c c

тогда

опре

=) As d becomes large, the diff. b/w

d' & d'' becomes

Very

small & amplitudes as

Elos +

Eg

Ove

virtually

identical of differ only in
phase. (i)

> ▣

22

22

Eodo

| Fode 23 |

Fade | 26

|End)

d'

d'

dir

evaluated at some time,

-feed is
evaluated

Fodo

=>

of

the

received E-field

is

say

$t =$

$d'' : / c,$

Epot

Eodo

d'

Eodo

LOO

Eodo

d'

d''

d

Eode

[200-1

]

Exor (d, t = 2'') = Fade
(en (ove ("d'')) - Enda (or
0°

d''

Eodo

d''

Etot

Os

Eodo

d'

1

Ерижи

ВЕТЬ

lent

Eo do

d'

Exon

Eodo

d''

I

Cas Os=

Si Os

D

[ENO
T)

=

∝

-

x

Eo do

d

Eodo

d

Eo do

x =

x²-

+

(Ti
de

Eodo

d

Eo do

d

todo Cas

(00)

d

Cool

Eo do Sin

(00)

de.

²
(- Eodo +

x)2 + y2

d'

Fodo Cas

d

²

²

y4

دارور

• $\text{CO}_2 + \text{SiO}_2$

$\text{CaSiO}_3 + \text{SiO}_2$

d

s

Fodo

2

$=$

2-26s03

d

$\text{CaSiO}_3 + \text{SiO}_2$

"1

Fodo

d

Fodo

d

$$2 (1 - \cos \theta)$$

V. Dsix Os

Fodo 2 Si

d

when θ

WHT,

éla

θ

$\ll 0.3$ radians

~ 2 Eode

(00)

Етот да Eodo

00 = 02 =
2710

=

4π hthe
π

dd

92

बहते

$$\begin{aligned} +0.3 &=) 0 \\ &=) 01 = \\ &0.6 \end{aligned}$$

E

[

[to smill
values 10,
Sino ~]

(
2h+he
)

=)

d

Oo

IT hehe

dd

ها

wher

06

40.3

0.6 = 455 hehe

477h4h

=>

$d =$

21

0.61

eld

20he he λ

=>

ETOT (d) \approx

\sim

2 Fodo

d

add

$-K \ v/m$

d^2

ШКТ,

Pr =

Pt Gr Gq d²

(4)이 자

PiGi Ca

(20

hehe)

(4π)² =

d²

Pt GE Ge ho²²

he

d

d⁴

40dB / decade. The

Ak

large distances, the

received

power falls off

distance raised to the fourth power,

or at a

with

path

вольт

loss for the two

—
lay

rate

model car

of

be expressed in dB as,

$$\begin{aligned}
 PL \text{ (dB)} &= 40 \log d - (10 \log h_t \\
 &+ 0 \log b_a + 20 \log h_t + \mathbf{d \log h_a}
 \end{aligned}$$

a

BS + uses a

255 dB to

A mobile is located 5 km away from vertical $1/4$ monopole antenna with a receiver cellular radio signals. The E field at 1 km from

gain
of

is measured to be 10^{-3} V/m. The carrier

the Tx

for

the system is 900 MHz

HY

of K

used

Hy.

a) Find the length of effective aperture

frequen
cy

the
of

Rei
ng

antenna

b) Find the received power at the mobile wing the **two-**

ray **ground** reflection model

assuming the height of Tixing

the

antenna is som & Being antenna

som & Reing antenna in 1.5m
above

groun

d.

soln

(ato

Cuver T-R seperation, $d=5$ km

E-fiel

d

field at a
distance

of

961

-3 vlm

1 km = 10

Freq. of operation,
 $f = 200 \text{ MHz}$

$d_0 = 1$

3×10^8

$\delta =$

$\lambda = = = f$

900×10^6

$\approx 1 \text{ km}$

$=$

0.33 m

Alu

a) Length
of

the antenna, $\delta = \frac{1}{4} =$
 $0.38/4$

8.21.Can.

aperture of
antenna

Expectation

apective

3

Words (0.13)'

Ae

a

Ad2

435 (0 (033) "

0-016 m2

EAT (*d*) =

6) The total cluster

field,

2 Fodo Thehe

d

ad

22x10-3

$$\begin{aligned}
 & \frac{5 \times 10^3}{3} \quad (50) \\
 & = 2 \times 10^2 \times \left[\frac{21}{10} \right] \\
 & \quad (10)
 \end{aligned}$$

$$0.333(5 \times 10^3)$$

$$\begin{aligned}
 & 118.3 \times \\
 & 10^{-6} \\
 & \times \\
 & 10^{-6} \\
 & \text{V/m.}
 \end{aligned}$$

The received

power

at

a

distance

e

$$Pr(d) = 1212 Ae$$

=

12055

$$(112 - 1 \times 10 - 6) \times 2 \quad (0.016)$$

- 5.4 X10

13

U

W.

1-62

रु

122.68 dBwCon -92.68dBm

12.5

Link Budget Design

→ by writing path loss models to calculate

the received signal

level as

a

function

distance, it becomes
possible to predict

the SNR for mobile
communication system.

Log distance Path

Loss Model

=> Both theoretical & measurement based

indicate that

with distance.

=> The

measurement based

propagation model

received signal power
decreases logarithmically

average

average large
mole

path

low for an arbitrary
T-R

seperation is,

PL (d) &

^

n

-path

do

PL (dB) = PL

(do) + Lon Log (1)

CO

n

los component which indicates the rate at which the

path loes Increased

with distance, do

4300

do - close in

distance

Slab laman

reference

d- T-R seperation distance

Eindhon ment

Free

2

space

Ueban Qua

2.7-3.5

In building

LOS

shadowed webar

obsturched by
building

3-5

16-1.8

4-6

→ in large
coverage
Commonly

Are

smaller

cellular

sys

tems,

1 km rejerice
distances

100 m aim) are used.

used, whereas in microcellular systems, much
distances (such as

Log - normal

shadowing

distance

path

loes model does not comider the

be

=) The

Log

fact that the

surrounding

environmental

clutter

vastly different at two

diffrent locations having

T-R

seperation.

may

the same

=) Ar

ary

value

cy

d,

the

peeth

Lois PL (d) at a

particula

r

location is random & distributed
log-normally about the mean distance
dependent value. (i)

$$PL(d) [dB] = PL(d) + X_0$$

4

$$PL(d_0) +$$

Log normal (d)

+ X₀

do

$$P_x(d) \text{ [dBm]} = P_t \text{ [dBm]} - PL$$

$$(d) \text{ [dB]}$$

X₀ - Zero-mean Gaussian distributed random variable (in dB)

with standard deviation σ .

استه

A

=) The log-normal distribution describes the random shadowing

over

a

large number

measurement

effect which occur

of mean

locations which have the same T-R

separation, but have
different
level

clutter on

The propagation
path. This

phenomenon is referred
to as

normal
shadowing.

$\log-n$

e

that measured
signal

=>

Lo

g

name shadowing

implies

leads at a

specific T-R separation
have

a

Gaussian

=> The close ius

reference
e

distribution about the distance
dependent

mean

distance
e do,

do, the
path

ВОЛО

exponent n,

las model T-R

seperation.

for an

of the standard deviation & statistically describe the path

a specific

arbitrary

location having

=) In practice

the values

and I are

g

completed from

measured data

using

g

linear regression such
that **the** diff.

losses is
minimized

b/w the measured & estimated
of

path

in a

mean

squerre

sense

over a

vide

range

of

measwement

be used to

locations & T-R
seperations.

penction (egy) may the received rignal
 lead will particular
 level.

$$S \exp(-2x) dx =$$

$$1/2 [1 - \exp(-2x)]$$

=> The

The &- penction

а елая

determine the

peob. that

that

exceed for

fall

kelow)

a

The &-penction is
defined

$R(2) =$

$\frac{2\pi}{z}$

where

$Q(z) = -2(-2)$

The pestability that the
receased

density
function

as

$\Pr [Pa (d)$

yue]

(1

V- Pe (d)

=

&

signal.

leal well

excee

d

a certain value Γ can be calculated from the curulative

Ally

the **peob.** that the received rignal level will he

below Γ is

giver

by

$$P_X [Pald)]=$$

Q (Pa1d) -20)

دمة سامحيا

Jad

Lowe own

The d

414

3/4

LH RELESS
CRANDONEES

of

the
amplitudes,
phases

or

just

Fading @ rapid fluctuations

multipath delays of a
radio signal & Caused by
interference the two

but

Not

short period
of time

due to more versions.

the transmitted signal which arrive at the
receiver at slightly different times.

Small Scale Multipath Propagation

→

Multipath in radio channel creates small scale fading

Effects.

The

*

effects

are

are

Rapid changes

* Random

диффузия

диффузия

Doppler
shifts

in

signal strength **swed**
modulation due to
varying

by multipath
propagation

* Time Dispersion
(caused by
delays.

→ Due to relative motion between mobile & BS,
each

multipath
experiences

an

apparent shift is
frequency.

the mobile

This is called Doppler shift & is
directly proportional
to the
velocity of

of

w.rt direction

**Factors
influences**

=> Factors

direction

of

→ Multipath

Propagation

motion

az

arrival of multipath

Small Scale

Fading

*** The presence of reflecting objects
& scatterers**

is the channel creates a cons

in

**Constantly
changing
environment**

Feed

igral

the dissipates the signal energy in
amplitude phase +
time. Thus, the multiple
versions

respect

displaced

with

spatial

Overtaking

Speed

of

the mobile

g

али

to

one another is

time 7

&

The relative motion bl_w is + mobile results is

random

on each

be tue

movi
ng

freq

▪

g

or

towar

d

modulation due to different

doppler shifts

the multipath component. Doppler shift will

-ve

dependi
ng

a

on whether the mobile :

away
from

→ Sped of
surrounding
objects

the BS.

mabras

If objects in the radio channel are in motion, they endure time varying doppler shift

of

the

the

surrounding

objects

the mobile, then this

7

of

moves

On

at a

me

effects dominates small side

surrounding objects

in

Itepeeth
components.

greater rate
than

jade
y.

ects can be

igne
nd..

y

multipath
channel

→ Transmission Bandwidth
of the signal

g
úgnal bandwidth >
bandwidth

Otherwire, mention

*

F_f

Fixed
signal

of liked

amplitude

ay

signal will be distorted in time but will not fade much

over a

local area.

∩

signal bandwidth &
bandwidth

of multipath chann the signal
will change rapidly but

signal will not be distand in time

M

Paramet
ers

of

Mobile Multipath
channels

=>

=> Many meiltepath
channel parameters

derived

are

power delay
people. They

relative

to a

power
r

Are

required
ted

the

from as
plots of

as

a

function
of

excurs

delay with

respeck

fixed time delay
reference.

=> Time Dispersion

Parameters

* The **time** dispersive properties of wideband
multipath

are most commonly
quantified by

channels

mean excess

del
ay

* The

mean

excess

delay

propele

-- =

(e) at
rons

delay

their ex

delay
spread
(se).

is the

first

moment

of
power

$$\sum Ax^2$$

$$E_p (ex)$$

I_k

k

$$E \{ A x^2 \}$$

$$E p(x)$$

k

k

the central

g

*

where $P(z)$ - multipath
power delay profile.

The first

moment

When

delay spread is the
square root

the power delay
people
of

$$G^2 = \frac{2}{(E)^2}$$

Elite EP (en) to

Eau

k

{P (ek)

K

2

리
Typical values
of

Д

что

delay
spread

Ale

on

the order

us is outdoor mobile radio channels & on the order

MO

ur indoor radio channels.

مو

Д

✚

* The cons

delay spread &

mear

+ mear excers

delay the tempeal

are

defin

ed

a

from

Average of

+

average

d

single

PDP which is

or spatial

consecutive impulse response
measurement collected

over

a

local

ama

* The maximum excers

del

ay

(x dB)

g

the PDP is the

time delay during which multipath

energy falls to X dB below the maximum.

In other words, it is defined

as

Ex

d

Ex- to where to is first

arriving signal & #

delay at

which a

-max. EXCEED

is within

signal

(does

полтавізо

в Со

Rxed power

$\times dB$

cy

multipath
component

the strangest
arriving multipath

(does not
necessarily

necessarily arrive at
to)

KRMS

delay

Ries delay

spied.

246. чого

Max. Excers delay

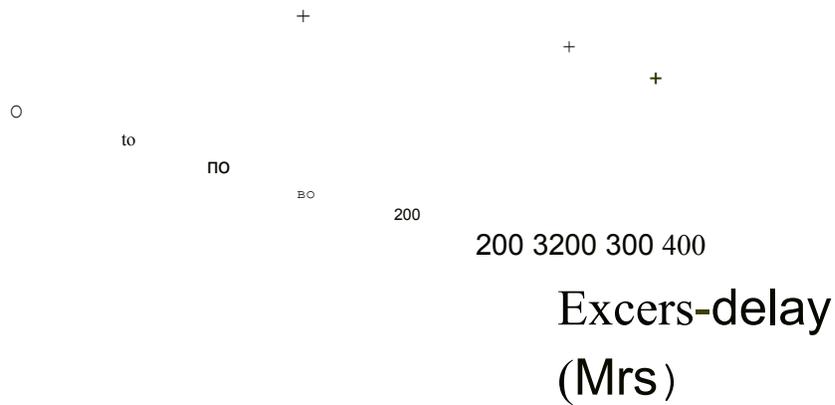
$$\langle [dB] = 84 \text{ Ad}$$

-20

-10

fe Mean Excels delay =
45.05 m

← Threshold
level = -2013



* in practice, values for Z,
ZZ & Je depend

cy

on the

choice

some threshold used to prevent P(c).

The noise threshold is used to differentiate multipath components & Thermal

if

TI

noise threshold is too low, the noise will be

4306

as multipath, giving rise to values

noise

processes

d

ce

Je that

Are

artificially

high.

Compute

the

ہیں

яТЬ

8

z, et

delay spread for the
following power

delay
people.

$P(e)$

0 μ s

صدق میرا

delay spread

Calculate &ms

Sol

$$E p (z a)$$

$$T a$$

==

K

روح
11

-

$$EP(4)$$

$$EP (z a)$$

$$T a 2$$

2

$$[(0) (0) +$$

$$\begin{pmatrix} 1 \\ 1 \end{pmatrix} + \begin{pmatrix} 1 \\ 0 \end{pmatrix}$$

1+1

31.5 us

$$\begin{pmatrix} 1 \\ 1 \end{pmatrix} + 2 \begin{pmatrix} 0 \\ 1 \end{pmatrix} + \begin{pmatrix} 1 \\ 0 \end{pmatrix}$$

انى =

{p(eu)

ما

2

1+1

$$25 - (1.5)^2 = 0.5 \text{ us}!$$

لرحمة

=25 us

→ Coherence
Bandwidth

* Coherence Bandwidth is derived
is the statistical
spread. It
is
of
frequencies

flat (\tilde{a}_0)
a

from

the

range

delay

y

the

g

range

statistical measure

over which the channel can be
considered

channel which passes all
spectral Components

with approx equal gain &
linear phase).

+ Two

*

Bc

Two sinusoids with freq. separation greater than B_c are

are

affected quite differently

If coherence

bandwidth is defined

as the bandwidth

over which the avg. correlation per cent is above 0.9,

$$B_c \approx 50 \frac{TE}{JE}$$

B_c

JE

of the freq- correlation is chosen to be

above 0.5,

Bc

Bc ~

1

se

Ther

Calculate the mean

excess

dela

y

rons

delay

spread +

the maximum excers

giver

delay (10 dB) for the multipath people

below: Estimate the
coherence

bandwidth

the channel, could this channel be suitable for
Aveps

AMPS

or CSM

revise without the use
of

ar

equaling
er?

OCB3Я

-codo

-2010

-30do

Pa(c)

2.

(مسد)

73

Soh

=> The

ぞ
とこ

200

ear

excers

delay is beads

mear

-Rods

-lods

$$(1)'(s) + (0.1)(2) + (0-1)$$

$$(1) + 0.01(0)$$

$$-0.01 + 01+0-1+!$$

o da

+0,01

0.1 0.1

4.38 us

=) The second

moment

احد

$$== (0.01) (0)^2 + (0-1) (1)^2 + (0-1) (2)^2 + (1) (5)^2$$

Ions delay

spread

$$0-01 +0-1 +0.1+1$$

Coherence Banded

th

=)

Bc

5 6e
1

Je =

と

|\u039b

= 21.07 us?

Trods bask

1.37 us

=
146 KH2

backwar alf

5(1.37.us)

wolle wethout .

ar

are

equalizer

:: Bc > 30k Hy, AMPS will

ASH requires 200KHy bandwidth
which

However

Exceeds Bc, thus

channel.

an

equalizer would be needed
for this

NA

استما

=> **Doppler Spread** ±

Coherence? Time

ere

*

Delay spread & coherence
bandwidth do not offer
information about
the time

native

of

the

varyi
ng

channel caused by either
relation motion between

the mobile & base station, θ
1

f

by

movement object in the channel.

Doppler spread & coherence

time

Are

nature

of

parameters which describe

the time varying

the channel \hat{u} a small-scale

small-scale region.

* Doppler spread B_D is a measure

of spectral broadening

caused by the time rate of change of the mobile

radio channel & is

defined

as

the range of

frequencies N_{D} which the received Doppler

spectrum is essentially

пол гелю

*

when a

$\rho \omega e$

serusoidal tone

3a of frequency f_e is Toud, the received signal specteun, called the Doppler specterem, will have components in the range $f_e \pm f_d$ to $f_e \pm f_d$, where

f_d

is

* The

which is

the Doppler shift.

The amount

a

of spectral broadening depends function of

relative velocity of

the angle θ b/w the direction

θ

& direction

g

directional

g

of

direction

on f_d

The mobile,
and

of

scattered waves.

the mobile

If

the baseband signal bandwidth is much greater than

Bo, the effects of
Doppler spread

Are

negligible at The
Rx.

This is a

slow

fade
channel

channel

Doppler

+ Coherence time T_c is the time domain dual

spread of B used to characterize the
time varying

of frequency

dispersiviners of

nature

the channel is time

domain. The doppler spread &

cohurence time

inversely

proportional to

be

122

fm

one

one

another

* Coherence time is a statistical measure

اوت

ان

the time duration

g

over which the channel impulse response is **invariant** of **quantifies the selectivity** of at different times.

*

of the reciprocal bandwidth

essentially

the channel

response

the baseband signal is
t

greater than the coherence time of the
channel, then the channel
will change during the
transmission

Causing distortion at the
receiver.

baseband

message,

thus

f

the coherence time
is defined

as the time ova

which

the time correlation
function

$$J_c = T_c \quad \rho$$

16 π

for

is above 0.5, then,

Where

•

for

$\Delta \tau$

dopple shift & mm =
old.

* Another popular
theems sule i

$\hat{c} =$

$\sqrt{\quad}$

935

baleant 0.423

$16\pi T$

Z_u

foo

Thus two signals
arriving with
than T_c

ale

Determine

make

that

a

time separation
greater

affected differently by
the channel.

the proper spacial sampling central required
to small scale propagation measurements
which assume Consecutive samples
highly correlated in time.
How

a

many samples will

2

1900
Meting
MHY

take

these

&

are

be
required

và

ove

com travel distance

1=50 mls . How long would it take

measurements, assuming they
could be made moving vehicle? what
is the Doppler

is real time from

if $f_e =$

to

\dot{u}

spread

d

Sob

една

B

B_0

for

Joe correlation

to $\text{Pic}/2$.

Pic =

167

7

16 при

=

ac

=

a

the channel ?

let time between samples is

ad

[:

fm = v / d]

16 пe

16πToge

[-id = c / fe]

паза

9x3x108

16xπ X 50 X 1900x106

=

565us

taking time samples at has
 then Ate half the sampling
 enterral is

π

$s_x =$

$50 \times 565 \text{ us}$

$= 1.41 \text{ cm.}$

B

Mo.

of

su

a

com travel
 distance

is

N_x

π

samples
 required

$$\frac{10}{DX} \times 141 \times 10^3 = \text{Jos samples.}$$

Time taker for their measurement

com
somlo
and
equal to
0.20.

The
Doppler
spread, $BD =$
for

Types

Small Scale Fading

$$\begin{aligned} & \text{c} = \text{sox (900 Xcb)} \\ & \text{3x cot} \\ & \text{6} \\ & \text{= 316,66} \\ & \text{Hay} \\ & \text{Hy} \end{aligned}$$

Fading Effect due to multipath
Time Delay **Spread**

* Had

Fading

of the mobile radio
channel has

linear phase

response over a

than the bandwidth

g

a

Constant
gain

वृ

दाय

bandwidth which is
greater

the food signal, then the
received

signed will undergo flat

fading.

Tixed rignal **is**
preserved.

The spectral chay of \rightarrow The shergth of
the received ignel charges wis time, due
to fluctuations **in** the gair of the
channel caused by

multiparh.

$s(t)$
 $s(t)$.

$x(t)$

$thi(te)$.

$h_{16,2}$

ясы)

t

t

Exx Is

1ste

k
1s

+ The
reciprocal

F
-5-
fe

bandwidth

Z

the transmitted signal
is

much larger than the multipath
time delay spread of the

channel + $\frac{1}{2} \lambda$, c)

can

excess

be

approxima
ted

ε

have
ry

no

delay (few a ringle detta
puction with $2=0$) .

→ Hat
fading

channels

channels (os) Narrowband
channels.

are also known

as

amplitude
varying

Fading

fast

g

channels cause

deep fades, &
outages

may require

20 a 30 dB more

transmitter power

to achieve low bit

error rates.

→ The distribution

distribution

of

instantaneous gain

of

flat fading channels is the Rayleigh

desteubution.

Thus

a rignal undergoes flat

fading if

$B_s \ll B_e$

κ

$A_s \gg J_e$

B_w

Pin-

Reciprocal B_u

Bandwidth

B_s

B_e

τ_{rms}

delay spread

B_c . Coherence Bandwidth

* Frequency

Selective Fading

phase

response

F

the channel

possesses a

constant

gain

4 linear

ove

a

bandwidth that is smaller than

frequen

cy

fadin

g

transmitted **signal**, then the
channel creates

the received
ungral.

the bandwidth

selective

on

→ The channel impulse response has multipath delay spread which is greater than the reciprocal bandwidth of the transmitted

Thus the

message.

Received signal includes multiple versions

the transmitted waves which are

no

attenuated &

delayed in time of hence the received signal is distorted. This & channel induces ISI, due to time dispersion of the transmitted signal with the channel.

→

Frequency
ency

Zara

selective fading channels
are much more difficult to model
than flat fading channels since
each multipath signal must be modeled &
the channel must be considered to be
a
linear
filter.

$s(t)$

$h(t, \epsilon)$

$w(t)$

0 1

t

t

حراء

f

ЯСН

ЯСН

To+e

The channel
becomes

frequ
ency

is different for different
frequency components.

→→ Frequency
selective fading

delays which
approach the
transmitted

selection, where
the gain

multipa
th

is caused

by or exceed the
symbol period

путв

o!

are also known as wideband
channels.

+Th
ey

Thus, a

signal undergoes
frequency

$Bs \quad y \quad Bc$

TS & TE

A rule

thumb:

Ÿ тpycote

selective
Jading of

→

• flat

jading

$T_s \ll T_E$ - freg. selective
Fading

⇒ Fading Effects due to Doppler Spread

* Fast Fading

وفل

→ In a fast Fading channel, the channel impulse Response changes rapidly within the symbol duration.

(e) the coherence

the channel is smaller than

the symbol period of

time

f

the transmitted
signal.

→ This causes frequency
despiciñas (also called time
selection jading) due to
Doppler spreading

→ Thus a

signal undayses

jait Jading i

$T_s > T$

à

$B_s \times B_D$

→ A flat fading, fast fading channel is

a channel in which
the
amplitude

late

the delta
penction

function
varies

%

faster than

the of change of transmitted
baseband signal.

→ In frequency **selective**, fast
fading channel, the
phases, & time
delays of any

one

аД

amplitu
des,

the multipath

8

Components vary faster than the rate of change of the Red synel.

* Slow
Fading

fadin
g

In slow

channel, the channel
impulse response

علم

changes at a rate much slower than

the transmitted
bandband signal
 $s(t)$.

→ The aloppler spread of the
channel **is** much less than
the bandwidth

This a

of

the baseband
signal.

upral undergoes slow
jading of rignal

lis xx

Pic

q

$B_s \gg BD$

Pransmitted
symol period

wad regnel

Бсю

Br

6e

Hat dow

Flat Fast

Fading

Fadin

g

Fung. Selective Treg.

selective

slow Fading Fast

Fadey

(

Fy selective 1 Frey.

Selective

slow

Fading

Fixed symbol
opened

Fast

Fading

Bc

Far Foot

Fat slow

Fadey

Fadin

g

Bs

Bd

Txed signal Bow

Small Scale

Fading

(Band

on

multipath time
delay spread)

CUCAL

Har Fadiy

Bw

Br

→ Bu of repnel LOW
& chanel

g

(Bs)

8

(Bc)

» Delay spead I symbol
peñad

(As)

(se)

Freq. selective
Feeding

=). Во у черпав у во3
channel

حمه جعبه لا

(Bs)

своју

=) Dday spread > symbol
perial

(TS)

Small - Scale
Fading

Doppler
Spread)

(Based on

Fast Fading

(ITC)

-) coherence time <
Symbol period

(a)

(se)

slov Jaday

2) Coherence teme >

Symso peñar

(c)

(Ts)